Design of a Wide Swath interferometric altimeter simulator for sea state bias estimation - OSTST 2010 - Lisboa

P. Dubois, L. Amarouche, J.C. Souyris, B. Chapron

18/10/10



OSTST 2010

Introduction

Scope of the work

Sea State Bias impact on the elevations measurements of the futur instruments : interferometric large swath Radar

- A quick introduction to the SWOT mission
- 2 Simulation principles
- The Sea Surface contribution
- 4 The Complex Signal calculation
- 5 Processing

A quick introduction to the SWOT mission 1/3

- Hydrology and Oceanography mission
- high spatial resolution global measurments of ocean surface topography
- 120 km wide swath with a +/- 10 km gap at the nadir track
- KaRin instrument
 - Ka Band 35.6 GHz



A quick introduction to the SWOT mission 2/3

The standard mode



A quick introduction to the SWOT mission 3/3

The ping pong mode



Simulation principles 1/3



Simulation principles 2/3

Even simple methods like the Kirchoff approximation suffer from intractable numerical burden when it comes to integrate large ocean surfaces (some km^2) at the radar wavelength resolution (some cm^2).

Our approach has been to adopt a two-scale integration scheme.

- The ocean surface is coarsely subdivided (1m scale pixels) and the elevation at this scale is explicitly integrated.
- The contribution coming from shorter scales within the pixels of resolution is accounted for in a statistical manner
- the pixel resolution is **not** linked to the radar resolution

Simulation principles 2/3





Resolution down to 1m

• Each patch is similar (in terms of elevations and slopes)

The Sea Surface contribution 1/2



P. Dubois (CLS/CNES)

OSTST 2010

(E) E ∽Q (0) 18/10/10 9 / 16

The Sea Surface contribution 2/2

- the LW and SW ocean power spectrum used are parts of the Unified Elfouhaily spectrum [Elfouhaily, 1997]
- the non linear transformation of the is carried out by the Choppy Wave Model [Nouguier 2009]
 - based on first order expansions of particle trajectories in Lagrangian coordinates.
 - expressed as an horizontal deformation of a reference linear surface, instead of vertical one as most weakly nonlinear models do
- the hydrodynamics modulations are carried out by the first order (linear) Modulation Transfer Function [Elfouhaily, 2001]

The Complex Signal calculation 1/2



P. Dubois (CLS/CNES)

OSTST 2010

<=> ■ つへで 18/10/10 11 / 16

The Complex Signal calculation 2/2

$$W^{(pq)}(t) = \frac{i\lambda}{4\pi} \sum_{n} \frac{g_1^{(pq)} g_2^{(pq)}}{R_1 R_2} \mathbb{S} \,\,\delta\left(t - t_{AR} - \frac{f_D}{K}\right) e^{i\frac{f_D}{K}(kc - \pi f_D)} e^{-ik(R_1 + R_2)} \tag{1}$$

- the sum is made over all the pixels describing the surface
- g₁ and g₂ are the antenna gain of the emiting/receiving (rectangular) antennas (resp.)
- *R*₁ and *R*₂ are the distance from the emiting/receiving antennas (resp.) to the pixel
- \mathbb{S} caracterize the scattering $(\sigma = 4\pi |\mathbb{S}|^2)$
- *f*_D is the doppler frequency
- $\delta()$ is the dirac function : the impulse response is simulated by a convolution after the summation.

P. Dubois (CLS/CNES)

18/10/10

12 / 16

Processing 1/2



P. Dubois (CLS/CNES)

OSTST 2010

▲ ■ → ○ へ ○
18/10/10 13 / 16

Processing 2/2

- Misregistration decorrelation : Channel Corregistration
 - the sampling of the 2 antennas is different since the difference of the view of the scene by the two antennas
 - on board algorithm : phase ramp applied within the range compression block

$$e^{i(a\Delta d\omega(\pm T_d + n\Delta t))},$$
 (2)

- for the sake of simplicity, the corregistration is carried out during the attribution of the pixel to a range gate
- The geometrical decorrelation : Spectral shift
 - frequency shift due to slightly difference of the view of the scene by the two antennas
 - on board algorithm : phase ramp applied in the time domain

$$\sum_{i=1}^{\infty} \Delta \omega_s(\theta_i) t$$
 (3)

Image: Image:

the frequency shift $\Delta \omega_s(\theta_i)$ is a function of the incidence angle

e

Conclusions

- High resolution simulator
 - the modular design allows to compare different configurations and to isolate the effects of each new feature on the SSB.
 - the validation relies on the validation of the simulator in the conventionnal Ku configuration.
- Sea Surface validation in progress
- Possibility to test the impact of the on board processing on the SSB (coregistration)

Thank you for your attention

Bibiography

T. Elfouhaily, Chapron B., Katsaros K. Vandenmark D. A unified directionnal spectrum for long and short wind-driven waves, *J. Geophys. Res.*, 1997

T. Elfouhaily, Thompson D.R., Vandenmark D., Chapron B., Higher-order hydrodynamic modulation : theory and applications for ocean waves, *Proc. R. Soc. London*, 2001

F. Nouguier, Guerin C.A., Chapron B., "Choppy wave" model for nonlinear gravity waves, *J. Geophys. Res.*, 2009

M. Simard, Rodriguez E., Real-Time Processing Algorithm for Wide Swath Radar Interferometry of Ocean Surface, *Geoscience and Remote Sensing Symposium*, 2006. IGARSS 2006

3 K K 3 K